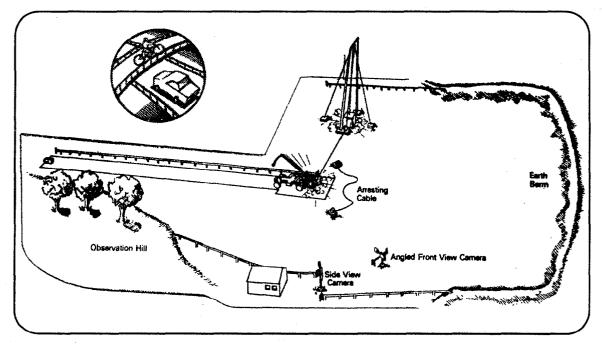
Crash Test Between a 6-KG/M

U-Channel Sign Support and a 1997

Geo Metro: FOIL Test Number 99F010

PUBLICATION NO. FHWA-RD-01-046

MARCH 2001



FOIL



U.S. Department of Transportation

Federal Highway Administration

Research, Development, and Technology Turner-Fairbank Highway Research Center 6300 Georgetown Pike McLean, VA 22101-2296

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FOREWORD

This report documents the results from one crash test between a 1997 Geo Metro two-door hatchback and a single-leg 6-kg/m u-channel sign support. The Federal Highway Administration (FHWA) has invested many resources in the development of finite element models (FEM) of passenger vehicles, pickup trucks, and roadside safety hardware. Computer simulations using these FEMs of collisions between the vehicles and roadside safety hardware are used to investigate the behavior of and improve the safety performance of roadside safety hardware. An essential step for developing the FEM is to validate the model by comparing data from simulation output with data collected from full-scale vehicle crash tests with roadside safety hardware. The FHWA's Federal Outdoor Impact Laboratory (FOIL) was used to conduct this test to develop and validate an FEM of the Geo Metro. nominal test speed for the test was 100 km/h and the nominal test weight of the test vehicle was 820 kg.

This report (FHWA-RD-01-046) contains test data, photographs taken with high-speed film, and a summary of the test results.

This report will be of interest to all State departments of transportation; FHWA headquarters; region and division personnel; and highway safety researchers interested in the crash worthiness of roadside safety hardware.

Michael Trentacoste, Director Office of Safety and Traffic

Operations Research and Development

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16. Abstract

This report contains the test procedures followed and test results from one crash test between a 1997 Geo Metro and a single-leg small sign support. test was conducted at the Federal Highway Administration's (FHWA) Federal Outdoor Impact Laboratory (FOIL) located at the Turner-Fairbank Highway Research Center (TFHRC) in McLean, Virginia. The target test speed for the test was 100 km/h and the target test inertial weight was 820 kg. A dummy was not used in this crash test. The test was conducted to provide data for validating a finite element model (FEM) of a Geo Metro and to investigate the potential for windshield penetration by the sign support after fracture. Computer simulations using the latest FEMs of a Geo Metro indicated that windshield penetration was possible while striking a small sign support with a sign panel mounting height of 1,525 mm. The results from the test verified the simulation's prediction that if a Geo Metro struck this particular sign support design with these material properties there was a high probability of windshield penetration or severe windshield/roof damage. Because the post fractured, other important safety performance measures including predictability of device activation and longitudinal occupant impact velocity met the safety performance criteria specified in the National Cooperative Highway Research Program (NCHRP) Report 350, test designation 3-61. and high-speed film coverage will aid in the continuing evolution of the Geo Metro FEM.

Geo Metro, acceleration, FO occupant impact velocity, racceleration, NCHRP Report	No restrictions. This document is available to the public through the National Technical Information Service, Springfield, VA 22161.		
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		SI* (MC	DDERN ME	TRIC)	CONVE	RSION FACTO	DRS
	APPROXIMATE CO	NVERSIONS T	O SI UNITS			APPROXIMATE CO	NVERSIO
Symbol	When You Know	M ultiply By	To Find	Symbol	Symbol	When You Know	Multiply
		LENGTH					LENGTH
in ft yd mi	inches feet yards miles	25.4 0.305 0.914 1.61	millimeters 'meters meters kilometers	mm 'm m km	mm m m km	millimeters meters meters kilometers	0.039 3.28 1.09 0.621
		AREA					AREA
in² ft² yd² ac mi²	square inches square feet square yards acres square miles	645.2 0.093 0.836 0.405 2.59	square millimeters square meters square meters hectares square kilometers	mm² m² m² ha km²	mm² m² m² ha km²	square millimeters square meters square meters hectares square kilometers	0.0016 10.764 1.195 2.47 0.386 VOLUME
fi oz gal fi ³ yd ³	fluid ounces gallons cubic feet cubic yards	29.57 3.785 0.028 0.765	milliliters liters cubic meters cubic meters	mL L m³ m³	mL L m³ m³	milliliters liters cubic meters cubic meters	0.034 0.264 35.71 1.307
NOTE:	Volumes greater than 100		n m³.	,			
		MASS					MASS
oz Ib T	ounces pounds short tons (2000 lb)	28.35 0.454 0.907	grams kilograms megagrams (or "metric ton")	g kg Mg (or "t")	g kg Mg (or "t")	grams kilograms megagrams (or "metric ton")	0.035 2.202 1.103
	TEMPER	RATURE (exact)		(0, 1)	(= /	•	ERATURE
۰F	Fahrenheit temperature	5(F-32)/9 or (F-32)/1.8	Celcius temperature	ဇ	°C	Celcius temperature	1.8C + 3
	ILLU	MINATION				· <u> </u>	LUMINAT
fc fl	foot-candles foot-Lamberts	10.76 3.426	lux candela/m²	lx cd/m²	lx cd/m²	lux candela/m²	0.0929 0.2919
	FORCE and Pf	RESSURE or ST	RESS			FORCE and	PRESSUF
lbf lbf/in²	poundforce poundforce per square inch	4.45 6.89	newtons kilopascals	N kPa	N kPa	newtons kilopascals	0.225 0.145

^{*} SI is the symbol for the International System of Units. Appropriate rounding should be made to comply with Section 4 of ASTM E380.

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SCOPE

This report documents the procedures followed and the results from one crash test conducted at the Federal Outdoor Impact Laboratory (FOIL) located at the Turner-Fairbank Highway Research Center (TFHRC) in McLean, Virginia. The test involved a 1997 Geo Metro two-door hatchback traveling at 100 km/h and a single-leg 6-kg/m sign support mounted in a strong soil. The test was conducted to provide actual crash test data for verifying the results from finite element computer simulations investigating variation in sign support safety performance as a function of sign mounting height. The simulation efforts were conducted by the National Crash Analysis Center (NCAC).

The results indicate that, for this particular sign post and vehicle combination, a mounting height of 1.5 m led to windshield contact by the sign panel during a collision. However, other calculated safety performance values were below the allowable safety performance criteria for sign supports outlined in the National Cooperative Highway Research Program Report 350 (NCHRP Report 350). (1)

TEST MATRIX

One crash test was performed on a 6-kg/m sign support. The test was conducted in accordance with NCHRP Report 350 test designation 3-61. Test designation 3-61 outlines parameters for a safety performance test of support structures involving an 820C (820-kg) vehicle striking a support at 100 km/h with an impact angle of 0° to 20°. Table 1 summarizes the nominal test conditions for test 99F010. The target impact location was center-of-post aligned with the vehicle's longitudinal centerline.

Table 1. Summary o	f nominal test conditions.
Test number	99F010
Test date	12-17-99
Vehicle	1997 Geo Metro
Nominal vehicle weight	820 kg
Nominal speed	100 km/h
Impact angle	0°
Support	6 kg/m u-channel (hat-section)
Soil	FOIL strong soil pit, Virginia 21A
Embedment depth	1,220 mm
Impact location	Vehicle centerline

VEHICLE

The test vehicle used was a 1997 Geo Metro LSi two-door hatchback with an automatic transmission. Prior to the test, the vehicle was drained of all fluids and its curb weight recorded. The vehicle's inertial properties were then measured using the FOIL inertial measurement device (IMD). The vehicle was stripped of certain components (spare tire, rear seat, shifter linkage, etc.) and instrumented with data acquisition equipment, sensors, an automated brake system, a high-speed film camera, and vehicle guidance equipment. The final vehicle test weight was determined and the vehicle's inertial properties were measured a second time as instrumented. The target vehicle inertial weight was 820 kg. A dummy was not used for this test. No components were removed from the vehicle's engine compartment. The battery remained in a charged state and connected to the power harness. The key was placed in the "start" position to activate air-bag power. summarizes the test vehicle's inertial properties and figure 1 lists the vehicle's physical parameters.

	Table 2	. Iner	tial prop	perties	of 19	997 Geo	Metro.	<u> </u>
Test Number	Weight (kg)	Height (mm)*	Long.cg ** (mm)	Pitch kg•m²	Roll kg•m²	Yaw kg•m²	Bumper Height (mm)	Wheel Base (mm)
		C-	urb Weight	Configu	ıration			-1
99F010	812	538	862	1,019	246	1,108	455	2360
		Tes	t Configur	ation (i	nertia	L)		
99F010	835	543	831	1,022	243	1,101	455	2360
* Height of vehicle center-of-gravity. ** Longitudinal center-of-gravity, distance behind front axle.								

DATE: 1	2-17-99 TEST	NO: 99F01	0 TIRE PRESSU	RE: 35 psi	MAKE: GEO	
MODEL: M	ETRO YEAR:	1997	ODOMETER:	·	GVW:	
TIRE SIZE:	155/80 R13 VIN N	UMBER: 2C1	MR2296V6760556		TREAD TYPE:	
MASS DISTRI	BUTION: CURB:	LF	265 RF	251 LR	143 RR 153	
	TEST IN	ERTIAL: LF	276 RF	265 LR_	149 RR 145	-
DESCRIBE AN	IY DAMAGE TO VEH					
N WHEEL.			VEHICLE CENTER	C WEEL	ENGINE TYPE: 1.3L 4 CYL. ENGINE CID: TRANSMISSION TYPE: X_AUTO MANUAL OPTIONAL EQUIPMENT:	
					AIR CONDITIONING	_
TIRE DIA WHEEL DIA	P Q G G G	- c - F	H H	D	Radio Driver and passenger Air Bags DUMMY DATA: TYPE: None MASS: SEAT POSITION:	_
GEOMETRY						
A 1525	E <u>591</u>	J <u>718</u>	N <u>1385</u>	R		
B 830	F <u>3785</u>	K 502	0 <u>1351</u>	s		
C2363	G <u>831</u>	L 106	P <u>577</u>	T		
D <u>1415</u>	н538	M <u>410</u>	Q <u>361</u>	<u> </u>	Name	
MASS	CURB	TEST INERTIAL	GROSS STATIC			
M_1	516	541	541			
M ₂	296	294	294			
M _T	812	835	835	1 ngi :	= 6.89 kPa	
	,			T POT	J. J. ILL G	

Figure 1. Vehicle properties for test 99F010.

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TEST DEVICE

The device tested at the FOIL was a single-leg small sign support buried in NCHRP Report 350 S1 strong soil. The sign support was constructed from one 6-kg/m u-channel hat-section and a 650-mm square aluminum sheet. The u-channel was cut to length (3,660 mm) and the sign panel was attached 1,525 mm above the ground line. The assembled sign support was placed in a 1,220-mm hole within the FOIL strong soil (crush-and-run) pit. The hole was back filled and compacted in 305-mm increments until ground level was reached. The sign panel was attached to the sign post using two 9-mm hardware quality bolts. A flat round washer was placed under the bolt head and nut.

Figure 2 illustrates the sign support installation. Refer to figures 7 and 8 in Appendix A for photographs of the test installation. Appendix C contains a stress-strain curve for the sign post material. The material testing was performed on specimens taken from the actual sign post tested. The material testing was conducted by the NCAC.

INSTRUMENTATION

Speed-trap, accelerometer, and high-speed film data were collected during the sign support test.

Speed trap. A speed trap was used to determine the vehicle's speed just prior to contact with the sign support. The center of the speed trap was located approximately 4 m before the sign support. The speed trap consisted of a set of five contact switches fastened to the runway in 305-mm intervals. As the vehicle passed over the switches, electronic pulses were recorded on analog tape.

Transducer data. The instrumentation used during the test consisted of a tri-axial accelerometer and a tri-axial angular rate transducer at the vehicle's center-of-gravity (c.g.). The data from the transducers were recorded by two data acquisition systems: the Diversified Technical Systems TDAS PRO onboard data acquisition system (TDAS PRO) and an umbilical cable tape recorder system. Table 3 describes the instrumentation used during the test. A three-dimensional sensor location is included in table 3. The location coordinates were referenced from the right-front wheel hub, which was 265 mm above ground.

The TDAS PRO is a self-contained system. The output from the sensors was filtered, digitally sampled, and digitally stored within the TDAS 8-channel modules mounted directly to the test vehicle inside the occupant compartment. The TDAS PRO system was set with a 3000-Hz analog pre filter and a digital sampling rate of 12,500 Hz. C.g. acceleration data, windshield data, and rate transducer data were collected via the TDAS PRO system.

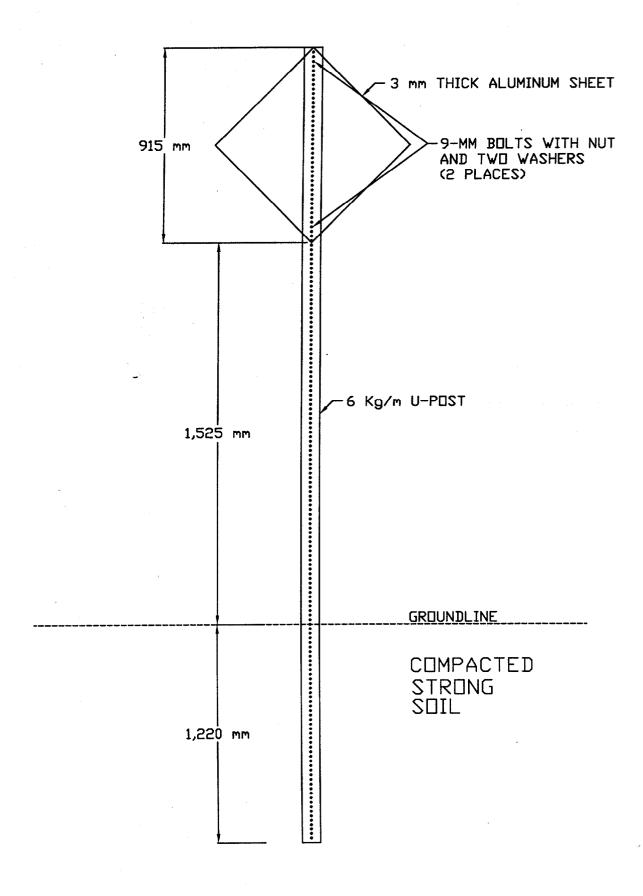


Figure 2. Sketch of small sign support.

The FOIL umbilical cable system utilizes a 90-m cable between the vehicle transducers and a rack of signal conditioning amplifiers. The output from the amplifiers was recorded on 25-mm magnetic tape via a Honeywell 5600E tape recorder. After the test, the tape is played back through anti-aliasing filters (set to 3000 Hz), then input to a Data Translation analog-to-digital converter (ADC). The sample rate was set to 12,500 Hz. The umbilical cable system recorded c.g. acceleration data.

	Table 3. Summary of instrumentation and channel assignments for test 99F010.					
	TDAS PRO onboard data system					
Ch	Transducer	Maximum range	Data description	Location* (X,Y,Z) mm		
1	Accelerometer	100 g	Vehicle c.g., X-axis	-800,750,140		
2	Accelerometer	100 g	Vehicle c.g., Y-axis	-800,750,140		
3	Accelerometer	100 g	Vehicle c.g., Z-axis	-800,750,140		
4	Accelerometer	200 g	Roof-windshield	-930,725,1,025		
5	Rate transducer	500 °/s	Pitch rate, c.g.	-800,750,140		
6	Rate transducer	500 °/s	Roll rate, c.g.	-800,750,140		
7	Rate transducer	500 °/s	Yaw rate, c.g.	-800,750,140		
	Umbili	cal cable,	tape recorder sys	stem.		
1	Accelerometer	100 g	Vehicle c.g., X-axis	-800,750,140		
2	Accelerometer	100 g	Vehicle c.g., Y- axis	-800,750,140		
3	Accelerometer	100 g	Vehicle c.g., Z- axis	-800,750,140		
11	Contact switch	1.5 V	Time of impact, TO	Not available		
12	Contact switches	1.5 V	Runway speed trap	Not available		
14	Generator	1.5 V	1 kHz reference signal	Not available		
* O:	rigin located at	right fro	ont wheel hub (265	mm above ground)		

High-speed photography. The crash test was photographed using seven high-speed cameras with an operating speed of 500 frames/s. All high-speed cameras used Kodak 2253 daylight film. In addition to the high-speed cameras, one real-time camera loaded with Kodak 7239 daylight film and two 35-mm still cameras were used to document the test. Table 4 summarizes the cameras used and their respective placements. The camera numbers listed in table 4 are shown in figure 3.

	Table 4. Summary of camera placement.					
Camera number	Туре	Film Lens speed (mm) frames/s		Location		
1	LOCAM II	500	10	Overhead		
2	LOCAM II	500	5.7	On-board, in vehicle		
3	LOCAM II	500	50	Right side 90° to impact		
4	LOCAM II	500	100	Right side 90° to impact		
5	LOCAM II	500	25	Right side 45°		
6	LOCAM II	500	150	Behind sign support in line with vehicle		
7	LOCAM II	500	100	Left side 45°		
8	BOLEX	24	ZOOM	Documentary		
9	CANNON A-1	still	ZOOM	Documentary		
10	CANNON A-1	still	ZOOM	Documentary		

DATA ANALYSIS

Data were collected via the FOIL analog tape recorder system, including speed-trap data, the FOIL TDAS PRO onboard data system, and high-speed film.

Speed trap. As the vehicle passed over the speed-trap tape switches, electronic pulses were recorded to analog tape. The tape was played back through a Data Translation ADC inside a desktop computer. The time between pulses was then determined using the software provided with the ADC. The time intervals between the first pulse and each of the subsequent four rulses together with the distances between corresponding tape switches were entered into a computer spreadsheet and a linear regression was performed to determine the best-line fit of the data points. The impact velocity was then determined from the slope of the best-line fit of the displacement vs. time curve.

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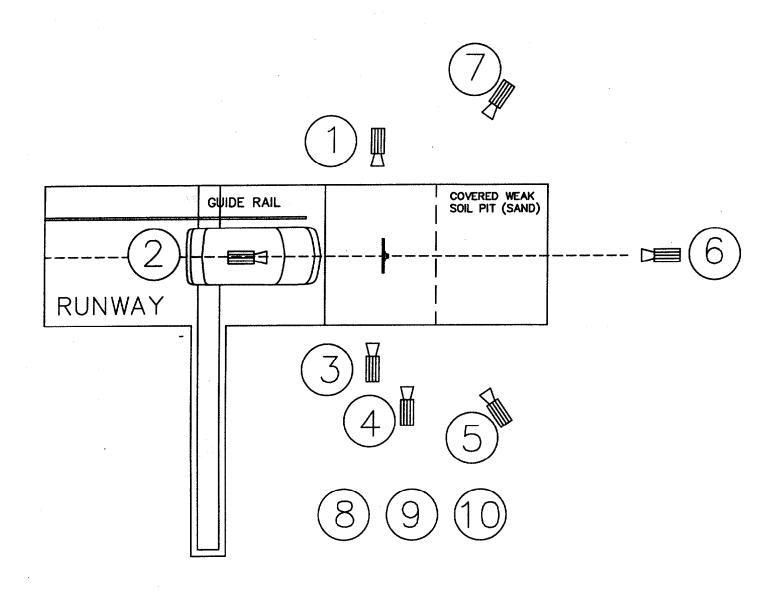


Figure 3. Camera placement, test 99F010.

Transducer data package. After the test, data from both data systems were converted to digital format and stored. The digital data from the tape recorder system and the TDAS PRO system were converted to the ASCII format, the zero bias was removed, and the data were digitally filtered using a digital Butterworth low-pass filter. The data from the crash test were digitally filtered with a cutoff frequency of 300 Hz (SAE J211 Class 180). The data were transferred to a spreadsheet for analysis.

The longitudinal c.g. acceleration data were integrated twice to produce velocity and displacement traces. Using techniques outlined in NCHRP Report 350 the occupant risk values were determined.

High-speed photography. The crash event was recorded on 16mm film by seven high-speed cameras. The film from the camera perpendicular to the vehicle trajectory, with a 50-mm lens, was analyzed for initial vehicle velocity. The overhead camera was used to verify the impact location, impact angle, exit angle, and exit speed. Analysis was performed using an NAC Film Motion Analyzer model 160-F in conjunction with a desktop personal computer. The motion analyzer digitized the 16-mm film, reducing the image to Cartesian coordinates. The Cartesian coordinate data were then imported into a computer spreadsheet for analysis. Using the Cartesian coordinate data, a displacement vs. time history was obtained. A linear regression was performed on the first 20 data points of the displacement vs. time traces to verify the vehicle's impact velocity. The film was used to verify data obtained from the speed trap and rate transducer and could be used in the event of transducer malfunction. was used to observe roll, pitch, and yaw angular displacements. The speed trap and accelerometer data were the primary data systems.

RESULTS

The Geo Metro was positioned on the runway and attached to The windows were up, the emergency the FOIL propulsion system. brake was released, and the ignition was in the "on" position to The vehicle was accelerated to 97.5 km/h activate the air-bags. prior to striking the small sign support. The vehicle made first contact with the sign post along the centerline as intended. vehicle bumper began to collapse on contact with the sign support. At 0.010 s after contact the bumper had been pushed back to the radiator while the sign post was slightly bowed and had begun to plow through the soil. The sign post and the plowing action imparted enough force on the vehicle to deploy the The vehicle continued forward and the sign air-bags (0.028 s). post fractured at approximately 0.40 s. The upper portion of the sign post rotated downward striking the vehicle at the windshield roof boundry. The vehicle passed over the sign stub and continued out into the FOIL runout area where the brakes were applied. The vehicle's bumper was torn from the vehicle prior to sign post fracture. The vehicle remained stable and upright. The vehicle came to rest after contact with the FOIL catch fence 101 m downstream from the impact location. Figure 4 summarizes the results from the small sign support test. Appendix A contains photographs of the test during the collision and the pre and post test environments. Table 5 lists the maximum and minimum peak values obtained from the vehicle accelerometers. The values listed are Class 180 data (digital filter cut-off frequency of 300 Hz). Appendix B contains data plots of the data collected from each vehicle sensor and velocity and displacement data plots created from the longitudinal cg acceleration trace. All acceleration data plots are from Class 180 data.

Table 5. Maximum and minimum peak values recorded.		
Location	Peak Acceleration (g's)	
	Max (+)	Max (-)
Cg X-axis	27.8	28.7
Cg X-axis, redundant	19.9	18.9
Cg Y-axis	10.6	15.9
Cg Y-axis, redundant	18.7	13.1
Cg Z-axis	29.1	27.7
Cg Z-axis, redundant	33.6	27.6
Windshield acceleration (peaks from data before sensor broke)	55.3	57.0

Occupant responses. The longitudinal occupant impact velocity (OIV) was determined to be 1.7 m/s and occurred approximately 0.4 s after initial contact between the vehicle and the sign support. The OIV value is below the limits specified in NCHRP Report 350. The longitudinal ridedown acceleration was below the allowable limits specified and was determined to be 0.4 g's.

<u>Vehicle damage.</u> Damage to the vehicle was extensive. The hood, roof, grill, head lights, and core supports were either crushed and/or dislodged from the vehicle. The bumper and lower front cross-member were torn from the vehicle. The windshield was shattered. Both air-bags were deployed.

<u>Sign damage.</u> The sign support fractured approximately 305 mm above ground. The remaining stub was bent backward and the sign

panel and post were launched downrange approximately 43 m. The trajectory of the sign post was in line with the vehicle trajectory. There was no evidence of post pull-out before fracture. The sign post could not be reused.

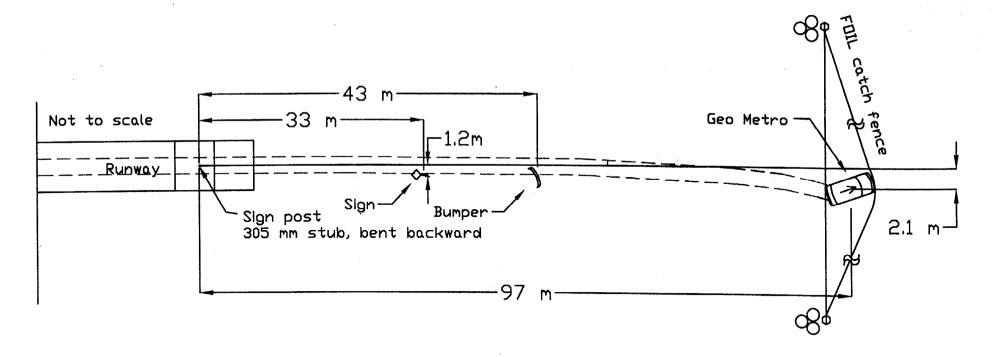
CONCLUSION

The data were successfully collected and the high-speed film successfully taken during the sign support test. The data and film will aid in the development and validation of a Geo Metro FEM and will help make sign mounting height recommendations. Computer simulations predicted that, for a sign support with these material properties, the sign support would strike a Geo Metro's windshield. The sign post fractured as anticipated and severely dented the vehicle's roof and shattered the windshield.

The results summarized in figure 4 indicate that the 6-kg/m small sign support embedded in strong soil did not meet the safety performance criteria outlined in NCHRP Report 350 (test designation 3-61). The sign support did fracture as anticipated and the longitudinal OIV (1.7 m/s) was below the allowable limit (5 m/s). However, the sign post contact with the vehicle caused a significant amount of denting to the roof and shattered the windshield, diminishing a driver's visibility. Table 6 summarizes the safety performance of the small sign support.

Table 6. Sign support safety performance summary.		
Evaluation Factor	Evaluation Criteria	Pass (P) or Fail (F)
Structural Adequacy	Test article should activate in a predictable manner.	P
Occupant Risk	Occupant compartment intrusion, debris hazard.	F, windshield and roof damgage
	Vehicle should remain upright and stable.	Р
	Longitudinal OIV (<5 m/s).	P, 1.7 m/s
	Longitudinal ridedown (<20 g's).	P, 0.4 g's
Vehicle Trajectory	Vehicle trajectory should not intrude into adjacent lanes.	Р
	Vehicle trajectory behind article is acceptable.	P

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Test locationFHWA FOIL Test number99F010	Occupant Risk:	<u>Observed</u>	Design/Limit
DateDecember 17, 1999	Longitudinal:		
Test designationNCHRP 350 test 3-61	Occupant delta V at 0.6 m	1.7 m/s	3/5 m/s
Test deviceSign support	Ridedown acceleration	0.4 g's	15/20 q's
PostsSingle leg 6-kg/m u-channel post	Lateral:	_	/ 5 +
Sign panel650-mm square aluminum sheet	Occupant Delta V at 0.3 m	no contact	NA
SoilCompacted 21A or crush-and-run Panel height	Ridedown acceleration	no contact	NA
Total height above ground2,440 mm	Peak 50 ms acceleration: Longitudinal	••••	3 3 0/0
FoundationEmbedded 1,220 mm in strong soil	Lateral		3.3 g s
	Vehicle Damage:		§
Vehicle1997 Geo Metro	Traffic Accident Data	(TAD)	12-FC-4
Weight: Inertial835 kg	Vehicle Damage Index	(VDI)	12FCEN3
Gross835 kg	Static crush		305 mm
DummyNo dummy	Post fracture	305	mm above ground
Impact speed97.5 km/h			-
Actual impact locationcenter	Exit speed		90.5 km/h
Impact angle0.0°	Exit angle	• • • • • • • • • • • • • • • • • • • •	· · · · · · · · · · · · 0 · 0 °

Figure 4. Summary of results, test 99F010.

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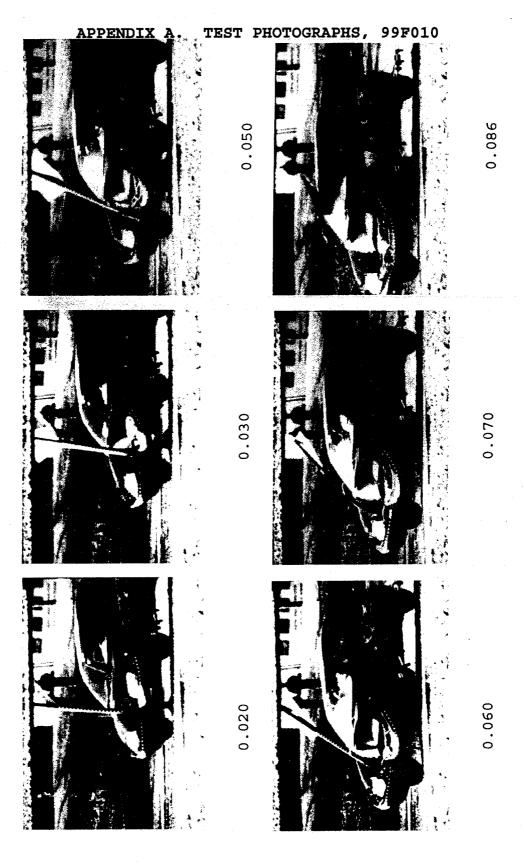
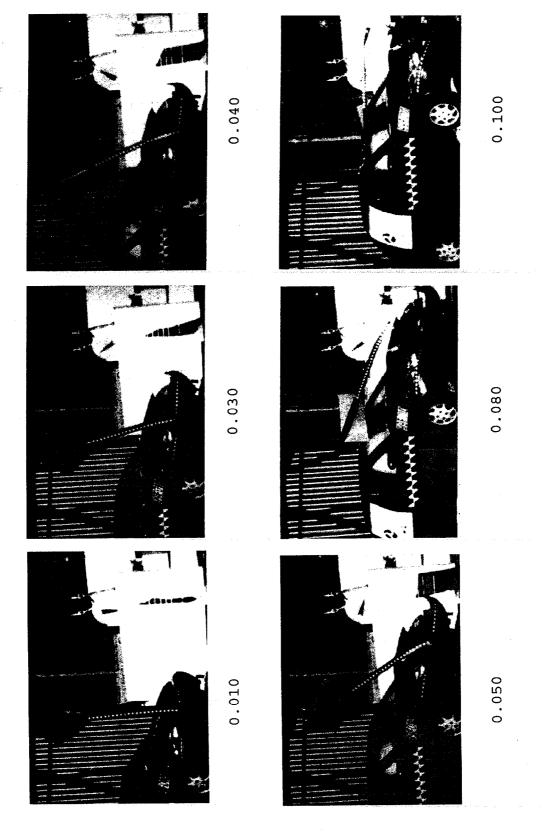


Figure 5. Photographs during the test, test 99F010.



Additional photographs during the test, test 99F010. Figure 6.



Figure 7. Pre-test photographs, test 99F010.

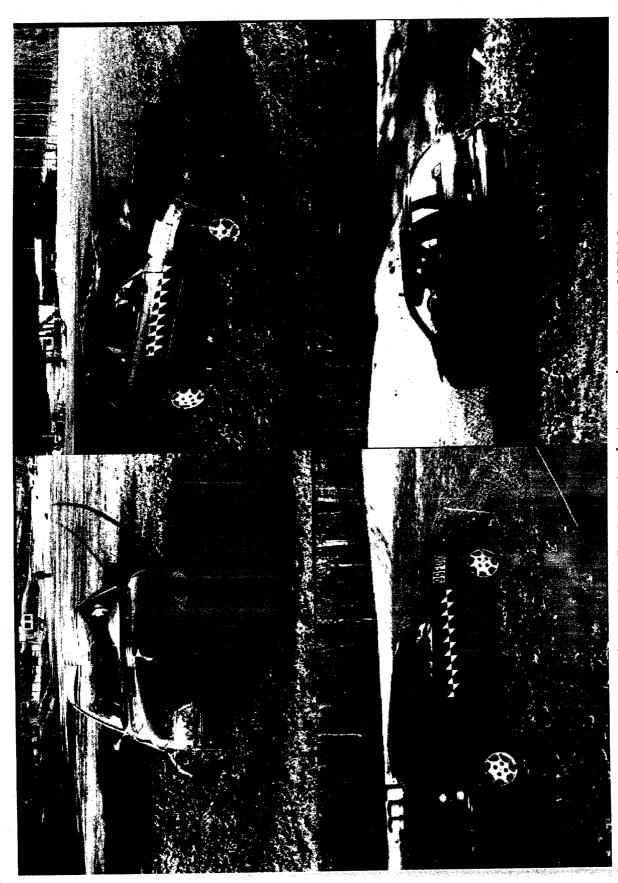


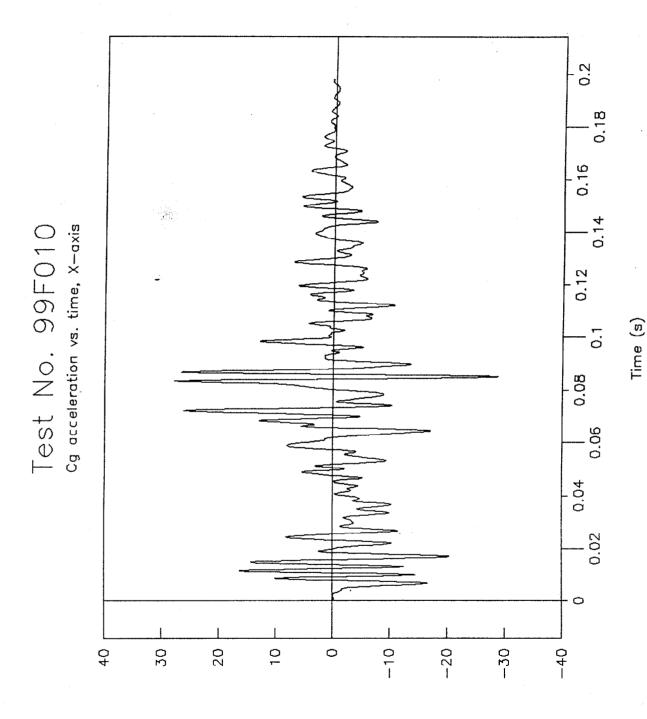
Figure 8. Post-test photographs, test 99F010.



Post-test photographs continued, test 99F010. Figure 9.

Figure 10. Additional post-test photographs,

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C.g. acceleration vs. time, X-axis, test 99F010. Figure 11.

Acceleration (g's)

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Acceleration (g's)

Test No. 99F010

Cg acceleration vs. time, extended

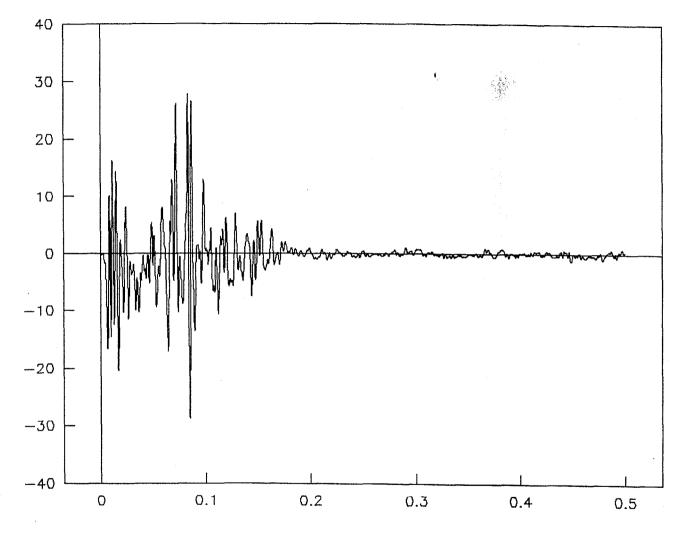


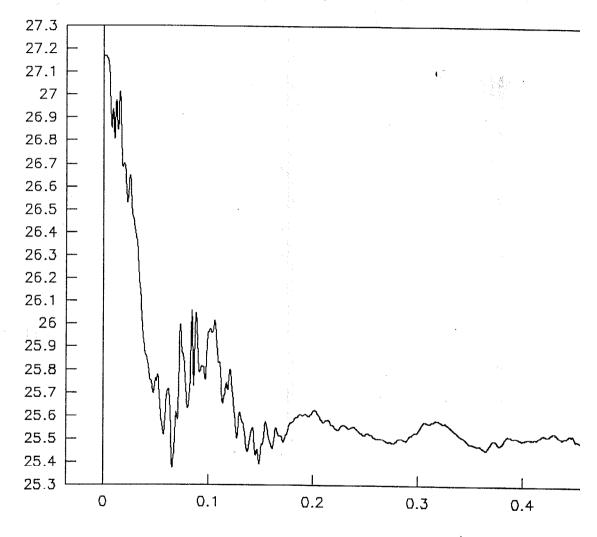
Figure 12. C.g. acceleration vs. time, X-axis extended, test 99F010.

Time (s)

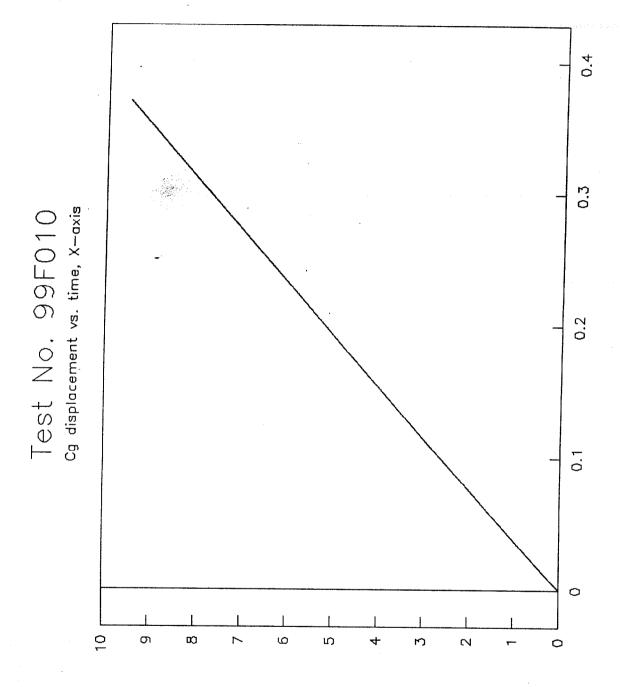
Velocity (m/s)

Test No. 99F010

Cg velocity vs. time, X—axis



Time (s)
Figure 13. C.g. velocity vs. time, X-axis, test 99F010



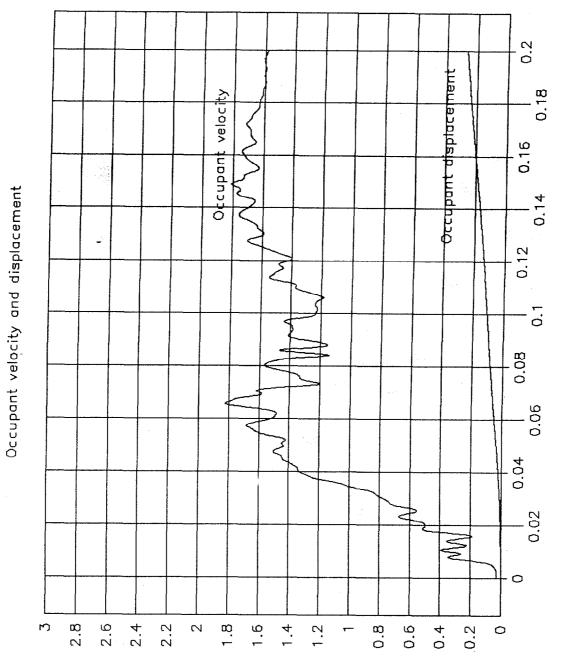
C.g. displacement vs. time, X-axis, test 99F010. Figure 14.

Time (s)

Displacement (m)

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Test No. 99F010



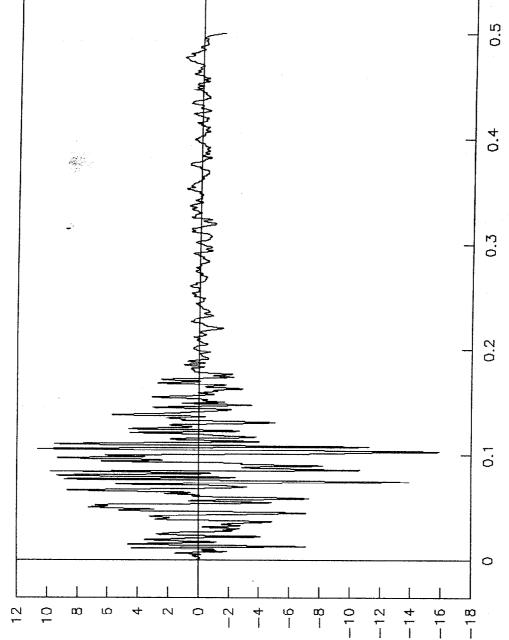
Occupant velocity (m/s) & disp. (m)

Figure 15. Longitudinal occupant velocity and displacement vs. time, test 99F010.

Time (s)

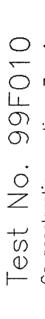
Test No. 99F010

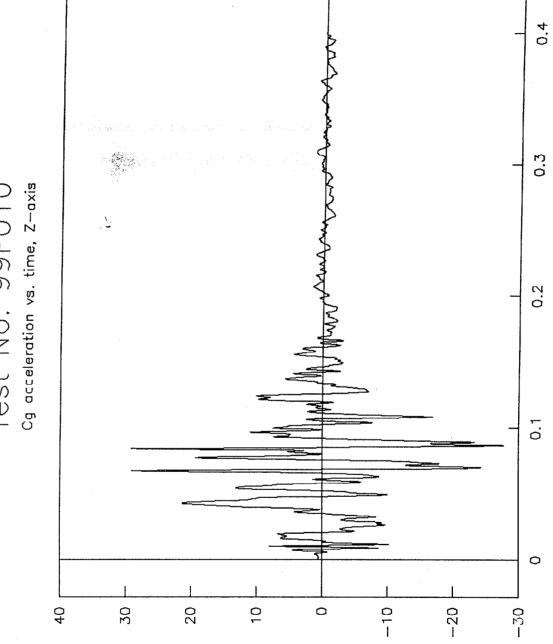
cg acceleration vs. time, Y-axis



C.g. acceleration vs. time, Y-axis, test 99F010. Time (s) Figure 16.

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C.g. acceleration vs. time, Z-axis, test 99F010. Figure 17.

Time (s)

Acceleration (g's)

Test No. 99F010

Acceleration vs. time, X—axis redundant

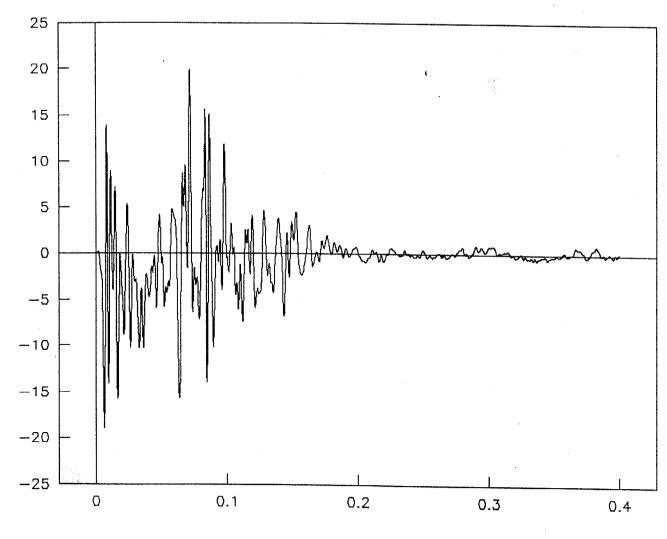
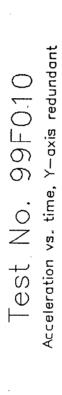
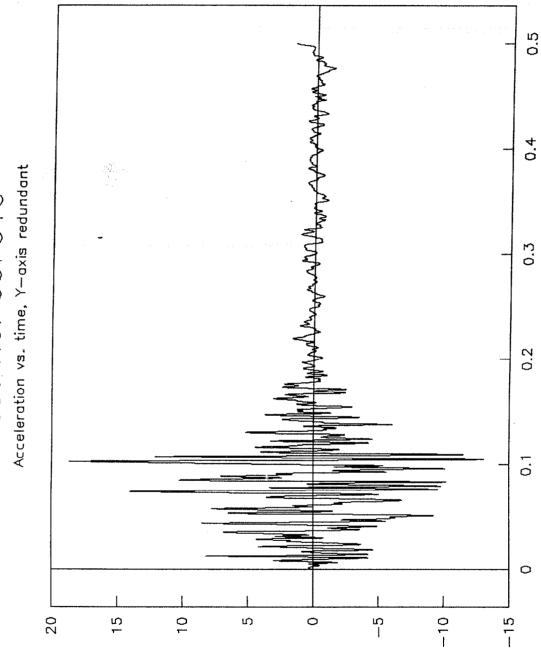


Figure 18. C.g. acceleration vs. time, X-axis redundant, test 99F010.

Time (s)

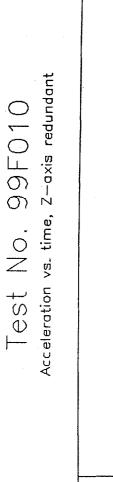


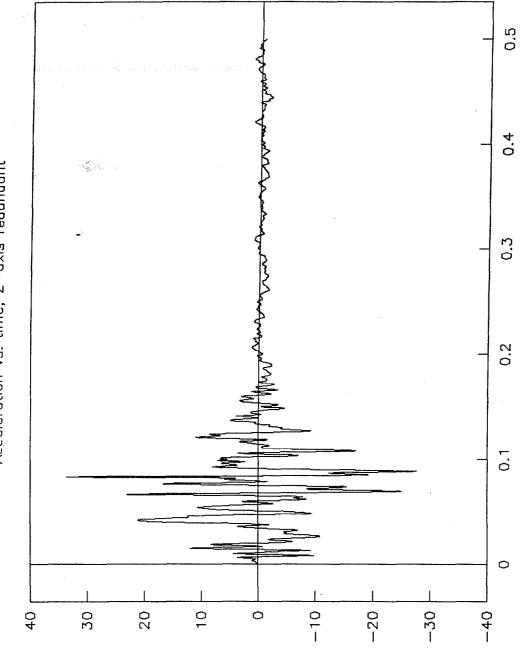


C.g. acceleration vs. time, Y-axis redundant, test 99F010. Figure 19.

Time (s)

Acceleration (g's)

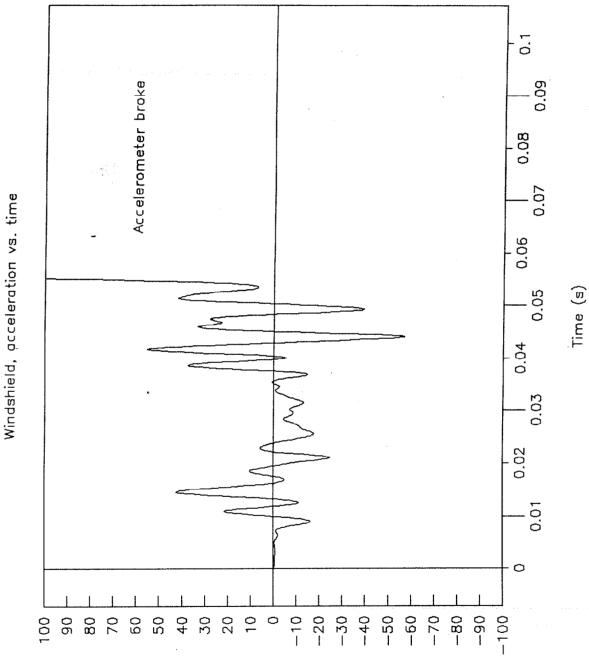




C.g. acceleration vs. time, Z-axis redundant, test 99F010. Time (s) Figure 20.

Acceleration (g's)

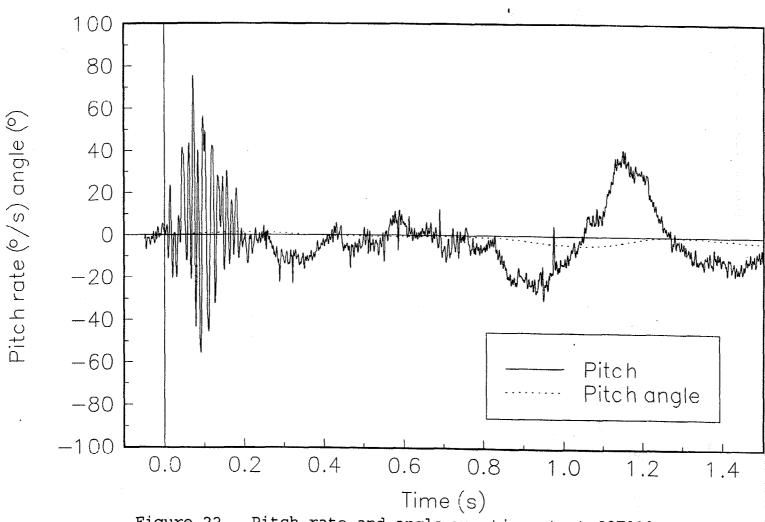
Test No. 99F010



Windshield accelerometer, acceleration vs. time, test 99F010. Figure 21.

Acceleration (9's)

Test No. 99F010 Pitch rate and angle vs. time



Pitch rate and angle vs. time, test 99F010. Figure 22.

Roll Roll angle Test No. 99F010 Roll rate and angle vs. time Time (s) 0.2 0.0 -200 200 100 -100Roll rate (\strut°) and angle (\strut°)

Figure 23. Roll rate and angle vs. time, test 99F010.

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Application of the sound of the Yaw Yaw angle Test No. 99F010 Yaw rate and angle vs. time -50

Yaw rate (\sqrt{s}) and angle $(^{\circ})$

Figure 24. Yaw rate and angle vs. time, test 99F010.

Time (s)

0.8

0.2

Engineering Stress-Strain Curve

Sign Post

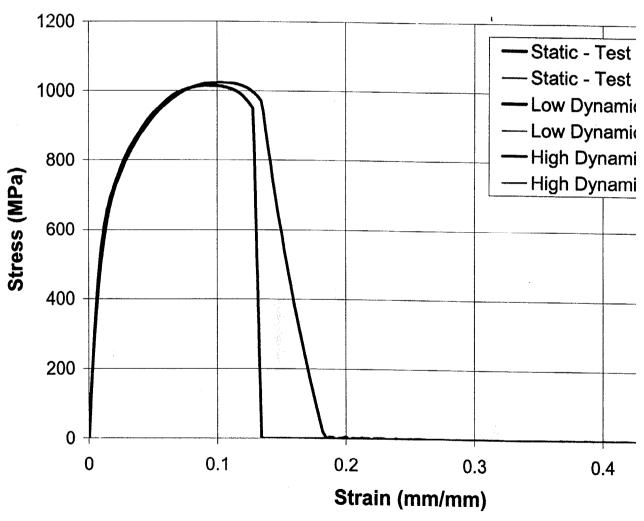


Figure 25. Engineering stress-strain curve for tested sign post,

REFERENCE

(1) Ross, H. E. Jr., Sicking, D. L., Zimmer, R. A., and Michie, J.D., Recommended Procedures for the Safety Performance Evaluation of Highway Features, NCHRP Report 350, National Cooperative Highway Research Program, Transportation Research Board, Washington, DC, 1993.